Amendments to the Specification:

Please replace the first paragraph of the Detailed Description of the Preferred Embodiment, page 2, with the following:

FIG. 1 presents component assembly 2 having a titanium part 4, a stainless steel part 6, and a filler material 8. Component assembly 2 is formed by brazing wherein it is heated to a specific process temperature that is below the melting point of titanium part 4 or of the melting point of stainless steel part 6, for a specific period of time, at a pressure that is created by force 10, that is exerted to place filler material 8 in intimate contact with the titanium part 4 and stainless steel part 6.

Please replace the first paragraph of the Detailed Description of the Preferred Embodiment, page 3, with the following:

The inventors prefer the term "laminated" versus other descriptive, but equally applicable, terms such as "layered", "clad", or "composite" material. The laminated filler material is not an "alloy" of nickel and titanium. An alloy, which is defined as a homogeneous mixture of two or more metals, where the atoms of one replace or occupy interstitial positions between the atoms of the other, of nickel and titanium, for example, does not demonstrate the depressed melting point that is available at a eutectic composition when nickel and titanium are in intimate contact. The laminate material supplies substantially pure nickel to initiate bonding with other metals, such as titanium or stainless steel, for example, at relatively low eutectic temperatures. For example, the lowest ~~liquidus~~ solidus temperature (also referred to herein as the melting point) in the nickel-titanium phase diagram occurs at 28% by weight nickel and is 942°C. Therefore, the optimum braze temperature will be greater than this temperature.